Carderock Division Naval Surface Warfare Center

AD-A268 605

Bethesda, Md. 20084-5000

CRDKNSWC-SSM-61-93/01 April 1993

Survivability, Structures, and Materials Directorate Research and Development Report

The Effect of Electric Discharge Machined Notches on the Fracture Toughness of Several Structural Alloys

J.A. Joyce, U.S. Naval Academy R.E. Link, Naval Surface Warfare Center





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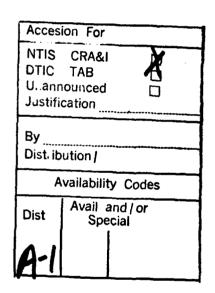
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ABSTRACT

Recent computational studies of the stress and strain fields at the tip of very sharp notches have shown that the stress and strain fields are very weakly dependent on the initial geometry of the notch once the notch has been blunted to a radius that is 6 to 10 times the initial root radius. It follows that if the fracture toughness of a material is sufficiently high so that fracture initiation does not occur in a specimen until the crack-tip opening displacement (CTOD) reaches a value from 6 to 10 times the size of the initial notch tip diameter, then the fracture toughness will be independent of whether a fatigue crack or a machined notch served as the initial crack.

In this experimental program the fracture toughness (J_{lc} and J resistance (J-R) curve, and CTOD) for several structural alloys was measured using specimens with conventional fatigue cracks and with EDM machined notches. The results of this program have shown, in fact, that most structural materials do not achieve initiation CTOD values on the order of 6 to 10 times the radius of even the smallest EDM notch tip presently achievable. It is found furthermore that tougher materials do not seem to be less dependent on the type of notch tip present. Some materials are shown to be much more dependent on the type of initial notch tip used, but no simple pattern is found that relates this observed dependence to the material strength, toughness, or strain hardening rate.

ADMINISTRATIVE INFORMATION

The work reported herein was performed at the U.S. Naval Academy and the Carderock Division, Naval Surface Warfare Center under the "Elastic-Plastic Fracture Mechanics of LWR Alloys Program," R.E. Link, Program Manager. The program is sponsored by the Office of Nuclear Regulatory Research of the U.S. Nuclear Regulatory Commission under Interagency Agreement RES-78-104. The Technical Program monitor is Dr. S.N. Malik at the USNRC. This effort was performed at CRDKNSWC under the supervision of Mr. T.W. Montemarano, Head, Fatigue and Fracture Branch (Code 614).

ACKNOWLEDGEMENT

This work was performed at the Naval Surface Warfare Center, and the U. S. Naval Academy, both in Annapolis Maryland, under the program, "Elastic-Plastic Fracture Evaluation of LWR Alloys," Mr. R.E. Link, Program Manager. The program is sponsored by the Office of Nuclear Regulatory Research of the U.S. Nuclear Regulatory Commission (NRC). The technical monitor for the NRC is Dr. Shah N.M. Malik. The authors would also like to acknowledge the help of Mr. Charles Roe of the Naval Surface Warfare Center and Mr. Wayne Farmer and Mr. John Hein of the U.S. Naval Academy.

1.0 OBJECTIVE

Standard techniques for evaluating the fracture toughness of a material involve testing a notched specimen that contains a real crack at the tip of the notch. The crack is introduced by fatigue loading the specimen at a load that is a small fraction of that required to initiate stable tearing. The fatigue cracking procedure results in a very sharp, natural crack that is designed to provide a high level of constraint and hence, a measurement of the fracture toughness near the lower bound. The fatigue cracking procedure can be a time-consuming process and adds to the cost and complexity of conducting fracture toughness tests. For many situations of practical interest such as the testing of weldments, it may be difficult, if not impossible, to produce a satisfactory fatigue crack that samples the material of interest. This is particularly true when trying to measure the fracture toughness of a heat affected zone or local brittle zone in a weldment. Residual stresses and inhomogeneity of material properties can lead to unsatisfactory crack fronts that do not sample the desired material or microstructure. Fracture toughness testing procedures could be greatly simplified if a very sharp, machined notch could be used as the initial crack in lieu of a real fatigue crack.

Conventional machining methods cannot produce a sharp enough notch that can adequately simulate a fatigue crack. Work by Joyce and Gudas[1] showed that machined notches with sharp tips (= 0.001 in. radius) but with included angles of 60° caused the measured J_k fracture toughness to be elevated by a factor of between three and four for an HY130 steel. Over the past decade, advances in electric discharge machining (EDM) equipment and procedures have made it possible to produce much narrower notches than previously available with notch tip radii on the order of 0.002 inches. It is a simple matter to produce slots in typical fracture specimens that are 0.004 in. wide with a 0.002 in. root radius at the tip of the notch. The advantage of an EDM notch over a fatigue crack is that the EDM notch can be located precisely at the microstructure of interest and the notch will be perfectly straight.

A basic assumption of elastic-plastic fracture mechanics is that a single parameter, the crack tip opening displacement (CTOD) or J integral is sufficient to describe the stress and strain distribution at the tip of a crack and that crack initiation occurs when this parameter attains a

critical value. The fracture toughness is defined as the critical value of this parameter at the onset of significant ductile crack extension. Recent computational studies of the stress and strain fields at the tip of sharp notches have shown that the stress and strain fields are very weakly dependent on the initial geometry of the notch once the notch has been blunted to a radius that is 6 to 10 times the initial root radius¹. It follows that if the fracture toughness of a material is sufficiently high so that fracture does not occur in a specimen until the CTOD reaches a value from 6 to 10 times the size of the initial notch tip diameter, then the fracture toughness will be independent of whether a fatigue crack or a smooth notch served as the initial crack.

The objective of this experimental program was to measure the fracture toughness, δ_i and J_{kr} and resistance curves (CTOD-R and J-R) for several structural alloys using specimens with conventional fatigue cracks and also with EDM notches. The results were then compared in terms of the ratio of the measured CTOD at crack initiation to the initial notch radius. It is expected from the preceding argument, that low toughness alloys will demonstrate a dependence of fracture toughness on the crack tip geometry, while tougher materials will not.

¹ Private communication, C.F. Shih, Brown University, USA, 1991.

2.0 EXPERIMENTAL DETAILS

2.1 Material Description

Six steel alloys and one aluminum alloy were examined in this investigation. Three of the steels were pressure vessel steels, ASTM A302, A533 Grade B, and A515. Two were high strength structural steels, HY-100 and ASTM A710 and the aluminum was a magnesium-molybdenum aluminum alloy, CS-19. This selection of alloys provides a wide range of strength and toughness with which to evaluate the effects of EDM notches on toughness. The aluminum alloy and HY-100 steel have a CTOD fracture toughness (using standard fatigue pre-cracked specimens) on the order of the EDM notch width used in this study. The remaining steels have a CTOD fracture toughness which is greater than the width of the EDM notch to varying degrees. The chemical composition and mechanical properties of the materials used in this study are listed in Table 1. The strain hardening exponent, N, was determined from the relationship²

$$\frac{UTS}{YS} = \frac{\left(\frac{n}{0.002}\right)^n}{\exp(n)} \tag{1}$$

where N=1/n.

2.2 Specimen Details

The specimen geometries used in this investigation were 1T C(T) and 1T SE(B) specimens. The C(T) specimens were used for the CS-19 aluminum and A710 steel and were 1 in. thick. SE(B) specimens were used for all other tests. The A302 and A515 steel specimens were 2 in. thick and the HY-100 and A533B steel specimens were 1 in. thick. All specimens were side grooved to a depth of 10% of the specimen thickness on each face. The SE(B) specimens had a flex bar mounted on one face of the specimen to measure the load-line displacement.

² Anderson, T.L. and Dodds, R.H., Jr., "Simple Constraint Corrections for Subsize Fracture Toughness Specimens," ASTM International Symposium on Small Specimen Test Techniques and Their Application to Nuclear Reactor Vessel Thermal Annealing and Plant Life Extension, January 29-30, 1992, New Orleans, LA.

Table 1 Chemical composition and mechanical properties of materials used in this study (Values are in weight percent).

	ASTM A302,Gr.B	ASTM A515,Gr.70	ASTM A533, Gr.B	HY-100	ASTM A710	CS-19
Carbon	0.18	0.28	0.19	0.16	0.04	•
Manganese	1.24	0.82	1.28	0.26	0.59	0.8
Phosphorus	0.012	0.009	0.012	0.003	0.005	•
Sulfur	0.023	0.028	0.013	0.009	0.004	•
Silicon	0.22	0.21	0.21	0.19	0.25	0.08
Nickel	•	•	0.64	2.78	0.90	•
Chromium	-	•	•	1.57	0.70	0.10
Molybdenum	0.47	•	0.55	0.42	0.19	•
Aluminum	-	•	-	•	•	Bal.
Iron	Bal.	Bal.	Bal.	Bal.	Bal.	0.07
Copper	•	•	•	•	1.17	•
Vanadium	•	•	•	0.003	0.003	•
Titanium	•	•	•	•	0.06	•
Columbium	•	•	-	•	0.03	•
Magnesium	-	•	•	•	•	8.42
Beryllium	-	•	•	•	•	0.001
0.2% YS, Mpa (ksi)	393 (57)	262 (38)	443 (64.7)	747 (109)	511 (74.6)	251 (36.4)
UTS, Mpa (ksi)	538 (78)	517 (75)	622 (90.8)	877 (128)	601 (87.7)	408 (59.2)
%Elon. in 50 mm (2 in.)	33	35	26	16.5	33	24
Red. of Area,	68	54	60	57	74	29
Hardening Exponent, N	9	5	9	15	15	7

Notches were prepared by wire electric discharge machining to extend the crack starter slot a minimum of 0.2 in., resulting in a final notch length, a/W, between 0.6 and 0.7. The wire diameter was 0.004 in. The EDM operation resulted in approximately semi-circular notch tips with a radius of 0.002 in. Photographs of the notch tip in a CS-19 aluminum and an A533B steel specimen are shown in Figure 1.

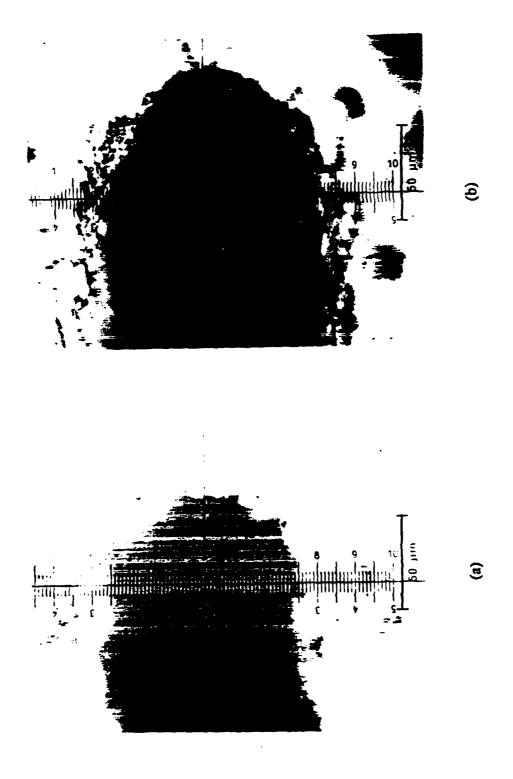
2.3 Test Procedure

Fracture toughness tests were conducted using the unloading compliance technique and following the guidelines in the relevant ASTM standards, E813, E1152 and E1290. The loading was carried out until a total crack extension of approximately 0.2 in. was achieved. Some results for the fatigue pre-cracked specimens were obtained from pre-existing data, and these had been tested to different final crack extensions. All data sets were analyzed using the equations and methods described in the following sections. J integral calculations were made using the crack growth corrected J equations of ASTM E1152, and these calculations are acceptable for J_k calculations according to ASTM E813. The CTOD (δ) calculations were made using two different equations so that comparisons between ASTM E1290 and the new ASTM Task Group E24.08.01 "Common Method" procedure could be made. In order to obtain the most accurate comparison of J_k and δ_i values, the initialization procedure that has recently been developed by ASTM Task Group E24.08.03⁴ was applied to all data. This procedure evaluates an average initial crack length that is then used for all crack extension estimations. This method avoids arbitrary "eyeball" data shifts that have characteristically been applied to J-R curves before evaluation of both J_k and δ_i values.

All testing was conducted at temperatures corresponding to the upper shelf for each

³"Standard Method for Measurement of Fracture Toughness," Draft 11, September 1992. Working document of ASTM Task Group E24.08.01, American Society for Testing and Materials, Philadelphia, PA 19103.

⁴"Standard Test Method for J-Integral Characterization of Fracture Toughness," Draft 8-4, January 1993, Working document of ASTM Task Group E24.08.03, American Society of Testing and Materials, Philadelphia, PA, 19103.



EDM notch tip geometry appearance in (a) CS-19 aluminum specimen and (b) A533B steel specimen. Figure 1

material. The HY-100, A710, A302 and CS-19 alloys were tested at room temperature. The A533B specimens were tested at 240°F and the A515 specimens were tested at 302°F.

3.0 ANALYSIS

3.1 Equations

The J resistance curves were calculated using the equations of E1152-87. The J integral was calculated using the relationship that:

$$J_{(0)} = \frac{K_{(0)}^{2}(1-v^{2})}{E} + J_{pk(0)}$$
 (2)

where K_0 is taken from Test Method E399-90 for the SE(B) specimen:

$$K_{(0)} = \left[\frac{P_1 S}{(BB_N)^{1/2} W^{3/2}}\right] f(a/W) \tag{3}$$

with:

$$f(a/W) = \frac{3(a/W)^{1/2}[1.99 - (a/W)(1-a/W)(2.15 - 3.93(a/W) + 2.7(a/W)^2)]}{2(1+2a/W)(1-a/W)^{3/2}}$$
(4)

and $K_{(i)}$ for the C(T) is:

$$K_{(0)} = \frac{P_i}{(B B_N W)^{1/2}} f(a/W)$$

with:

$$f(a/W) = (2 + a/W) \frac{[0.866 + 4.64a/W - 13.32(a/W)^2 + 14.72(a/W)^3 - 5.6(a/W)^4]}{(1 - a/W)^{3/2}}$$

For both the SE(B) and C(T) specimens:

$$J_{pl(j)} = \left[J_{pl(j-1)} + \left(\frac{\eta_i}{b_i}\right) \frac{A_{pl(j)} - A_{pl(j-1)}}{B_N}\right] \left[1 - \gamma_i \frac{(a_i - a_{i-1})}{b_i}\right]$$
(7)

where for the C(T) specimen:

$$\eta_i = 2.0 + 0.522$$
 b/W, and $\gamma_i = 1.0 + 0.76$ b/W,

and for the SE(B) specimen:

 $\eta_i = 2.0$ and $\gamma_i = 1.0$.

For CTOD calculations, individual δ values were calculated in two ways. For the ASTM E1290 δ calculations the equation used was:

$$\delta = \frac{K^2(1-v^2)}{2\sigma_{15}E} + \frac{r_p(W-a_0)v_{pi}}{r_p(W-a_0)+a_0+z}$$
 (8)

where the center of rotation is defined by r_p , with $r_p=0.44$ for the SE(B) and $r_p=0.4(1+\alpha)$ for the C(T) specimen with α defined by:

$$\alpha = 2\sqrt{\left(\frac{a_0}{b_0}\right)^2 + \frac{a_0}{b_0} + \frac{1}{2} - 2\left(\frac{a_0}{b_0} + \frac{1}{2}\right)}$$
(9)

and $v_{p(0)}$ is the plastic component of the crack mouth opening displacement measured at a distance z outside of the specimen crack surface. This equation estimates the crack tip opening displacement at the position of the original crack tip using the original crack length for all

calculations, i.e. for the calculation of K, r_{a} , and $b_{a} = (W - a_{a})$.

For the ASTM E24.08.01 "Common Method"⁵ δ calculations the equation used was:

$$\delta_{(0)} = \frac{K_{(0)}^{2}(1-v^{2})}{2\sigma_{m}E} + \frac{[r_{p}(W-a_{(0)}) + \Delta a]v_{p2(0)}}{[r_{p}(W-a_{(0)}) + a_{(0)} + z]}$$
(10)

with Δa being the crack extension that has occurred since the beginning of the test.

This "Common Method" equation is estimating the CTOD at the original crack tip using a specimen center of rotation that is adjusted to account for the true crack length as the test proceeds.

3.2 Analysis Methods

Values of the fracture toughness at the initiation of stable tearing, J_k and δ_i were determined for each specimen in accordance with the procedures in E813 and E1290, respectively. The J_k procedure of ASTM E813 involves a fit of a two parameter power law equation to the J-R curve data in an "exclusion zone" just beyond the point of ductile crack initiation, as shown in Figure 2. The J_Q point is evaluated from the intersection of this best-fit power law and an offset line as shown on Figure 2, and becomes J_k if specimen size and other criteria are satisfied. This method of evaluating J_k is very sensitive to value of the initial crack length used to estimate the crack extension of each data point on the J-R curve (or δ -R curve). The ASTM E813 method requires the use of a pre-test initial crack length, which often is not the best value to use for the evaluation of J_k . A new method has recently been developed by a

⁵ "Standard Test Method for Measurement of Fracture Toughness," Draft 11, September 1992. Working Document of ASTM Task Group E24.08.01, American Society for Testing and Materials, Philadelphia, PA 19103.

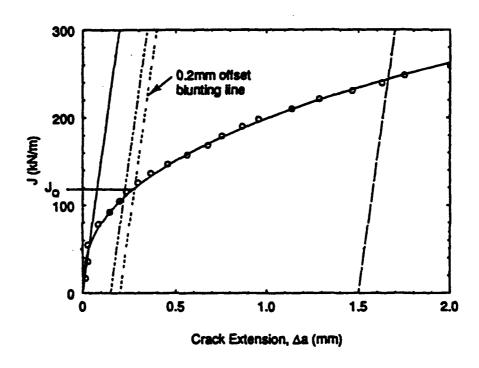


Figure 2 Schematic showing E813 procedure to obtain J_Q using an offset construction line procedure.

working group of ASTM Subcommittee E24.08.036 which fits a construction line to the initial J_i - a_i data to evaluate a best-fit average initial crack length for use in estimating Δa and hence the J-R curve and J_k . This procedure has been used for all results presented here. The schematic in Figure 3 shows how this method fits a "construction" line with the equation $J=2\sigma_i\Delta a$ to the J-R curve data with $0.2J_Q \leq J_i \leq 0.6J_Q$ and then extrapolates to the abscissa to evaluate a average initial crack length. This crack length is used for the evaluation of the J and δ resistance curves and then for the evaluation of J_k and δ_i .

The procedure for evaluating δ_i given in ASTM E1290 involves fitting a three-parameter power law to the initial region of the δ_i -R curve, as shown in Figure 4, and then evaluating the CTOD at a crack extension of 0.2 mm (0.008 in.) using a vertical line as shown in Figure 4. This procedure is simpler than the E813 J_k procedure described above, but it is even more sensitive to the initial crack length that is used to calculate the Δa_i values used to generate the δ -R curve. As discussed further below, this procedure has serious flaws, and often results in toughness measures that severely underestimate the true toughness of the material.

The Common Method Subcommittee has proposed an alternative procedure for determining the CTOD initiation fracture toughness for implementation in a common fracture toughness testing standard under development. The proposed procedure is very similar to the E813 J_{k} procedure with a two-parameter power law fit to the data near crack initiation and defines the initiation point as the intersection of the fitted curve with a line offset from the blunting line as in the procedure for J_{k} . A schematic of this method is shown in Figure 5. This value of CTOD has been denoted as δ_{iCM} (subscript CM for Common Method) in this report to distinguish it clearly from the E1290 δ_{i} quantity. One objective of the "Common Method" is to make this value of CTOD at "initiation" correspond to the J_{k} initiation point of the E813 procedure. In this work, correspondence is taken to mean that for a given specimen the J_{k} and

⁶"Standard Test Method for J-Integral Characterization of Fracture Toughness," Draft 12, March 1993, Working Document of ASTM Task Group E24.08.03, American Society for Testing and Materials, Philadelphia, PA, 19103.

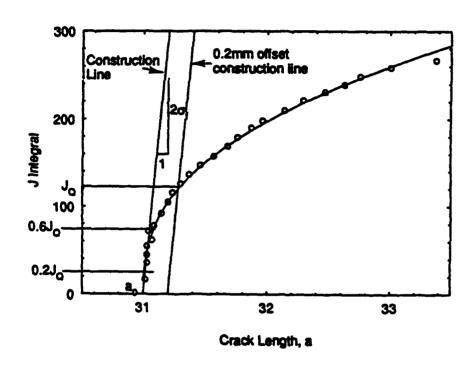


Figure 3 Schematic showing proposed procedure to evaluate the best initial crack length from unloading compliance results.

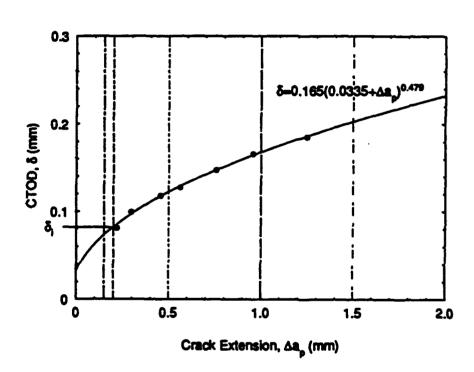


Figure 4 Schematic of E1290 procedure to obtain δ_i .

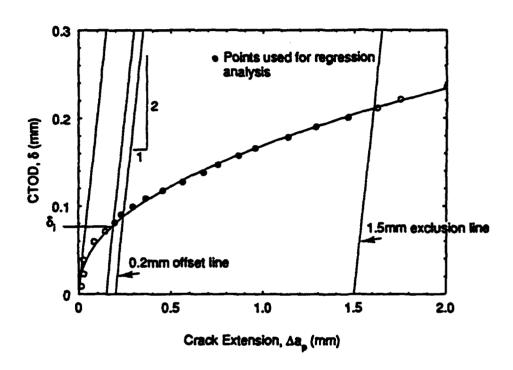


Figure 5 Schematic showing the Common Method offset construction line procedure used to obtain δ_i .

 δ_i values obtained would relate to the same amount of ductile crack extension. In a later section a modification of the Common Method is proposed which improves the correspondence of the J_k and δ_{iCM} crack initiation measures.

4.0 DISCUSSION OF RESULTS

4.1 Resistance Curve Results

J-integral resistance curves for EDM notched and fatigue cracked specimens are plotted in Figure 6-11 for each material. Detailed listings of the results from each test are included in Appendix A. A quick perusal of these figures shows that, as expected, some materials appear to be very sensitive to the type of notch used, while some materials are quite insensitive. Unfortunately, it does not appear that a simple toughness criteria amply predicts which materials are sensitive and which are not. CTOD resistance curves for the same set of specimens are presented in Figure 12-17 and they show exactly the same pattern as demonstrated by the J-R curves. In all cases the resistance curves of EDM specimens are elevated in comparison with the fatigue precracked specimens. In some instances, the elevation is small and the resistance curves overlap somewhat as shown by the A515 alloy while the A533B alloy shows a modest, but clear, elevation, and the CS-19 aluminum shows a dramatic effect, with an elevation by a factor of 3 at a given value of crack extension.

The material tearing resistance, defined as:

$$T_{\text{max}} = \frac{E}{\sigma_{\text{c}}^2} \frac{dJ}{da} \tag{11}$$

is evaluated for each material/notch geometry data set at a crack extension of 1 mm (0.039 in.) in Table 2. Both modest increases and decreases seem to result for the EDM notch geometry. The low toughness materials, HY-100 steel and CS-19 Aluminum show a 31% decrease and a 55% increase, respectively. The high toughness A710 alloy seems to be unaffected by the notch geometry, while the intermediate toughness materials are only modestly affected by the presence of the EDM notch. The numbers in Table 2, for instance, show a toughness decrease of 19% for the A515 steel, yet this does not seem justified looking at the J-R curves of Figure 7 which shows that considerable data scatter is present for the four specimens tested in this case. It appears that the data is too limited to make any clear conclusion except that no strong effect seems to be present when the fatigue crack is replaced by an EDM notch.

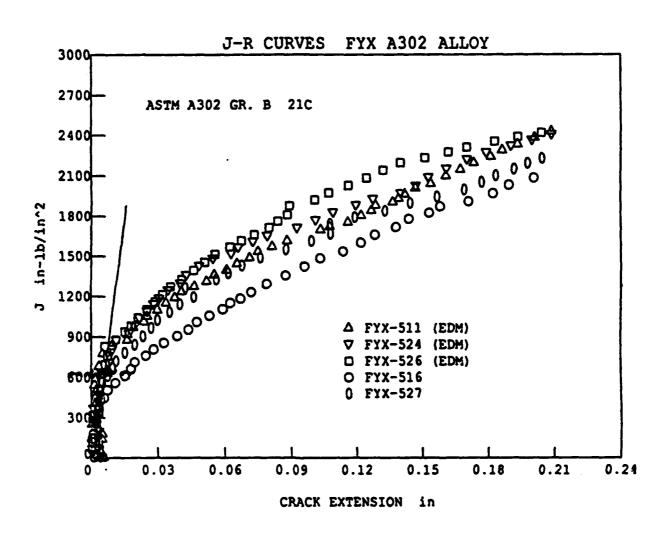


Figure 6 J-R curves for the ASTM A302 alloy showing EDM and fatigue precracked results.

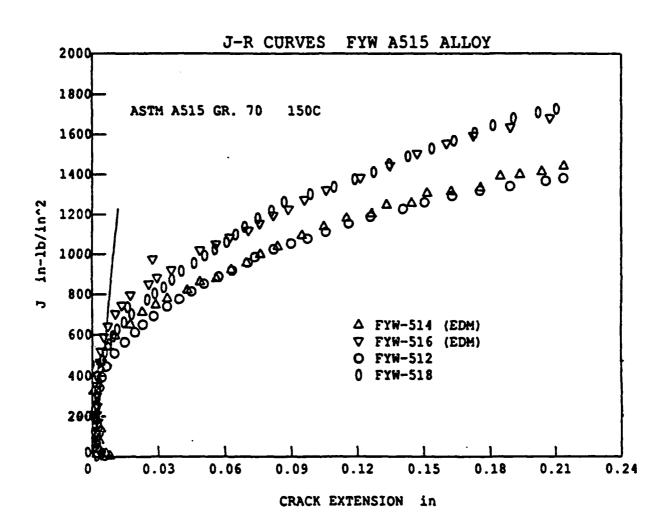


Figure 7 J-R curves for the ASTM A515 alloy showing EDM and fatigue precracked results.

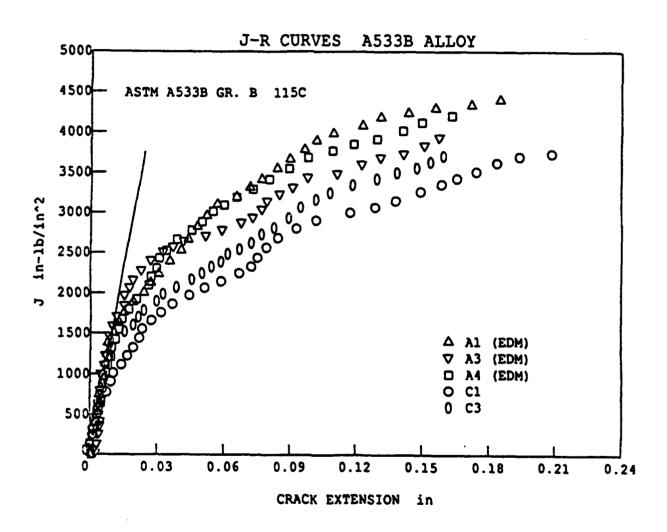


Figure 8 J-R curves for the ASTM A533B alloy showing EDM and fatigue precracked results.

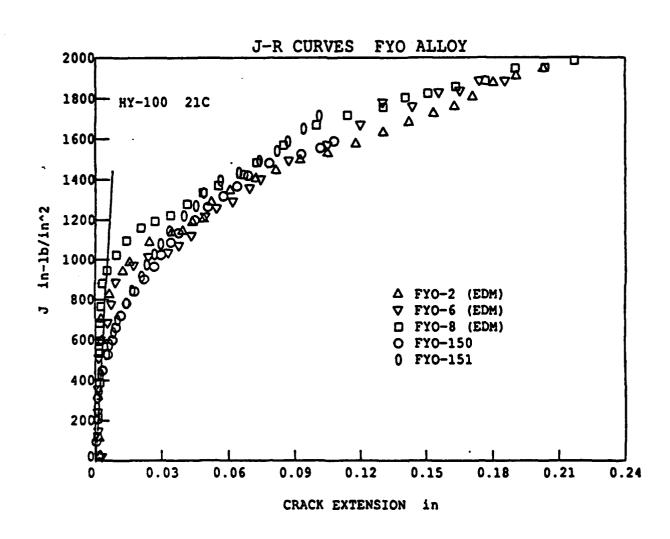


Figure 9 J-R curves for the HY-100 alloy showing EDM and fatigue precracked results.

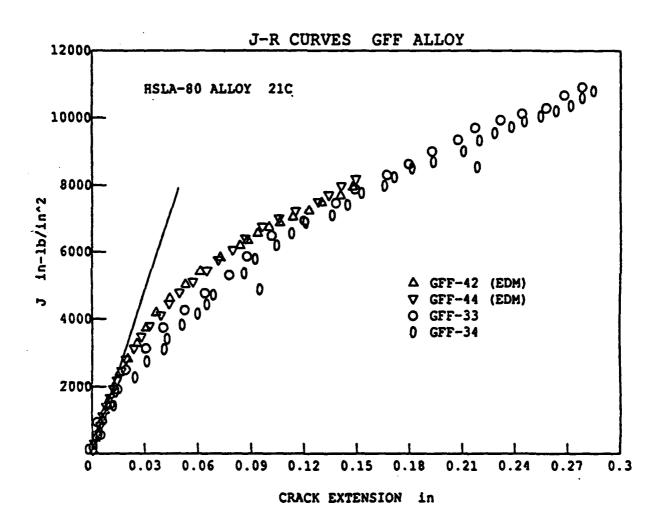


Figure 10 J-R curves for the ASTM A710 (HSLA-80) alloy showing EDM and fatigue precracked results.

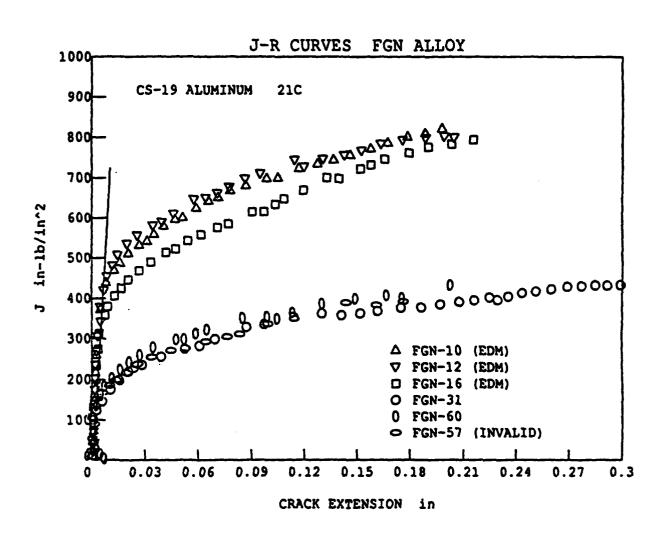


Figure 11 J-R curves for the CS-19 alloy showing EDM and fatigue precracked results.

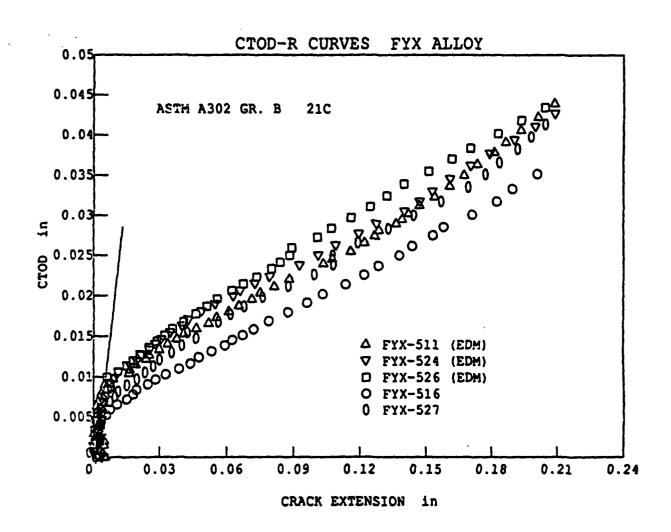


Figure 12 δ-R curves for the ASTM A302 alloy showing EDM and fatigue precracked results.

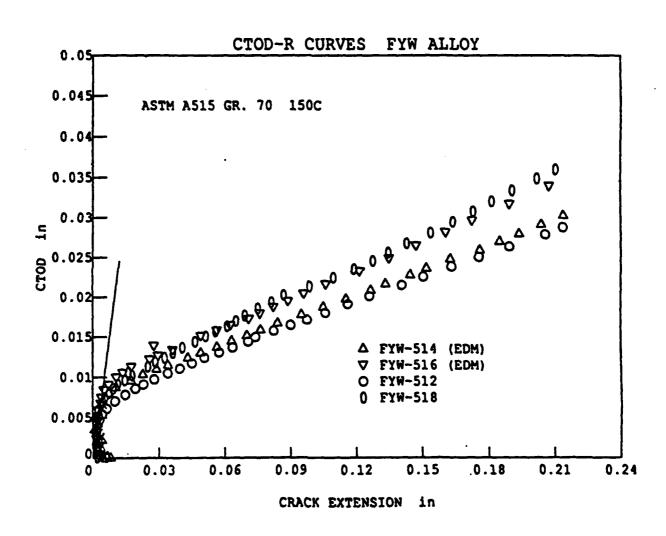


Figure 13 8-R curves for the ASTM A515 alloy showing EDM and fatigue precracked results.

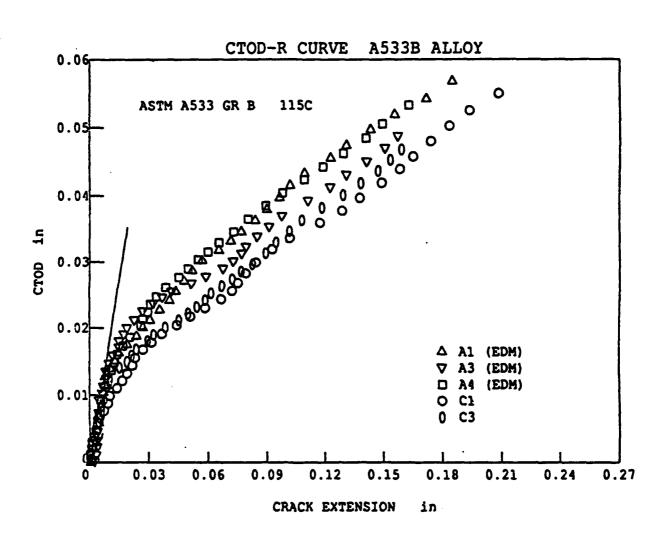


Figure 14 δ-R curves for the ASTM A533B alloy showing EDM and fatigue precracked results.

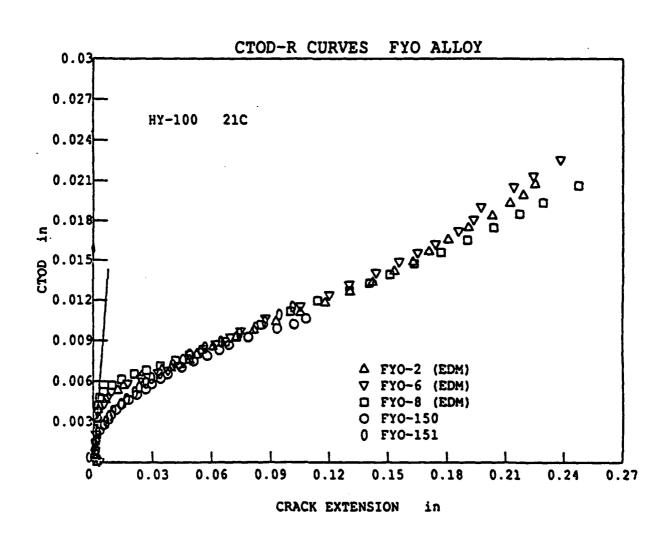


Figure 15 δ-R curves for the HY-100 alloy showing EDM and fatigue precracked results.

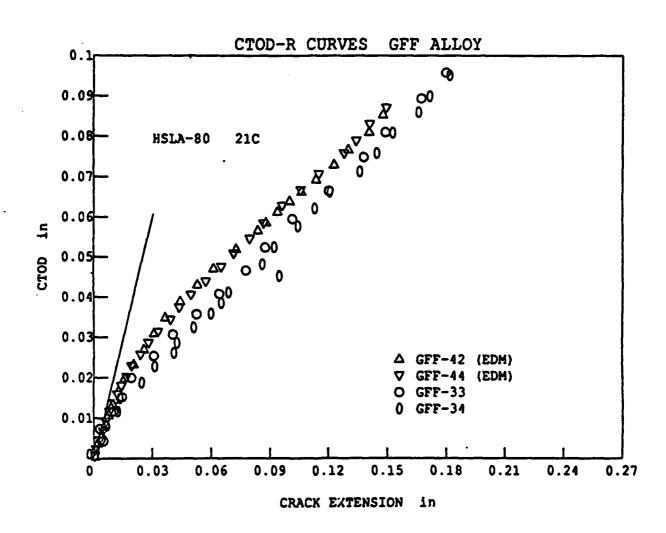


Figure 16 δ-R curves for the ASTM A710 (HSLA-80) alloy showing EDM and fatigue precracked results.

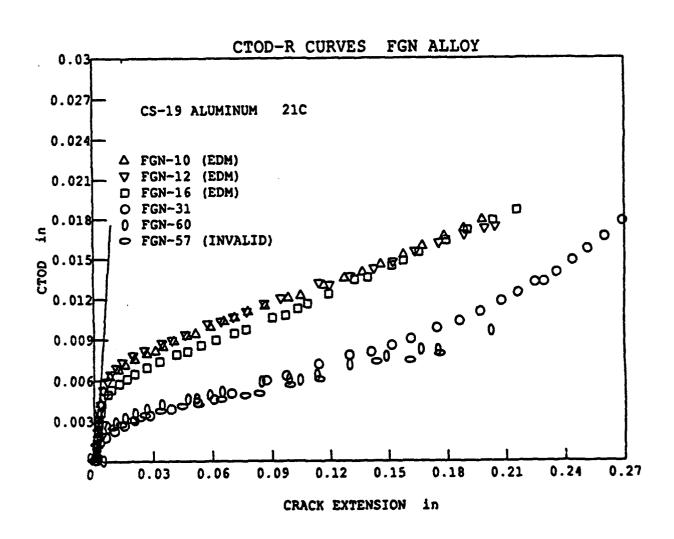


Figure 17 δ-R curves for the CS-19 alloy showing EDM and fatigue precracked results.

Table 2 Comparison of the average tearing modulus for fatigue precracked and EDM notched specimens.

	T et 1 mm.									
Material	Patigue	EDM	% 4 67.							
A302	134,	141.	5.2							
A515	134,	108.	-19.							
A533B	152	162.	6,6							
HY-100	46.5	32.	-31.							
A710	240.	240.	0.0							
CS-19	8.3	12.9	55 .							

4.2 Initiation Toughness Results

 $I_{\rm kr}$, $\delta_{\rm i}$, and $\delta_{\rm iCM}$, calculated as described in the previous section, are tabulated in Table 3. The analysis used for $I_{\rm kr}$ for specimen FYW-512 is shown in Figure 18, while the calculations of $\delta_{\rm i}$ and $\delta_{\rm iCM}$ are shown for the same specimen in Figure 19. The average values of fracture toughness for each material are tabulated in Table 4. Some material scatter is clearly present with $I_{\rm kr}$ values ranging by up to 17% from the average, $\delta_{\rm i}$ values ranging up to 12% from the average, and $\delta_{\rm iCM}$ values ranging up to 16% from the average. In all cases, the EDM notched specimens exhibited higher initiation toughness than the fatigue precracked specimens. The elevation in fracture toughness varied from 11% to 152%, depending on the material and specific measure of fracture toughness considered. As would be expected, the CTOD toughness designated in the Common Method is consistently higher than that measured according to ASTM E1290 and it ranks the materials in exactly the same fashion as does the $I_{\rm kr}$ measure of E813.

The E1290 definition of δ_i unfairly penalizes higher toughness materials that exhibit substantial crack tip blunting prior to tearing. This is clearly evident in the case of the ASTM A710 steel. The A710 steel had the highest J_k toughness of all materials tested. In terms of δ_i , the A710 ranked third in toughness, just below that of the A302 steel, which had a J_k of approximately one-third that of the A710. According to E1290, the critical event occurs at a fixed amount of crack extension, 0.008 in., regardless of whether the crack has actually begun to tear. The A710 steel is still exhibiting blunting behavior at this point, and as shown on

Table 3 Fracture toughness values for EDM notched and fatigue precracked specimens.

Material	Specimen ID	Notch Type	J _{la} (in-lb/in ²)	T at 1 mm	δ _ί (in.)	δ _{CM} (in.)	As at J _b (in.)	An et S _{eral} (in.)	Percent Diff. As
ASTM	FYX-511	EDM	864	128.	0.0090	0.0096	0.0145	0.0129	-11.0
A302 Gr. B	FYX-524	EDM	\$77	149.	0.0091	0.0099	0.0146	0.0131	-10.3
	FYX-526	EDM	913	147.	0.0098	0.0104	0.0148	0.0133	-10.1
	FYX-516	Fatigue	566	125.	0.0061	0.00621	0.0123	0.0112	-8.9
	FYX-527	Fetigue	730	144.	0.0072	0.00758	0.0135	0.0119	-11.9
ASTM	FYW-514	EDM	614	107.	0.0006	0.00847	0.0135	0.0123	-8.9
A515 Gr. 70	FYW-516	EDM	769	109.	0.0097	0.01032	0.0149	0.0133	-10.7
G. 70	FYW-512	Fetigue	534	128.	0.0068	0.00702	0.0128	0.0116	-9.4
	FYW-518	Fatigue	6 33	139.	0.0068	0.00909	0.0139	0.0127	-8.6
astm	A1	EDM	1834	208.	0.0122	0.0147	0.0198	0.0154	-22.2
A 533 Gr. B	A3	EDM	2287	106.	0.0148	0.0198	0.0227	0.0179	-21.1
۵	A4	EDM	2020	170.	0.0110	0.0169	0.0210	0.0165	-21.4
	C1	Fatigue	1292	156.	0.0084	0.0117	0.0163	0.0140	-14.1
	ය	Fetigue	1599	149.	0.0106	0.0135	0.0183	0.0148	-19.1
HY-100	FYO-2	EDM	929	32.6	0.0050	0.00507	0.0120	0.0106	-11.7
	FYO-6	EDM	847	35.3	0.0051	0.00472	0.0117	0.0105	-10.3
	PYO-8	EDM	1065	28.1	0.0058	0.00569	0.0126	0.0109	-13.5
	FYO-J3	Fatigue	748	38.1	0.0099	0.00385	0.0113	0.0100	-11.5
	FY0-J4	Fatigue	658	43.2	0.0038	0.00348	0.0109	0.0096	-10.1
	FYO-150	Fatigue	701	\$0.1	0.0034	0.00356	0.0111	0.0099	-10.9
	FYO-151	Petigue	715	\$4.6	0.0035	0.00363	0.0111	0.0099	-10.5
HSLA-80	GFF-42	EDM.	4063	229.	0.0097	0.0243	0.0339	0.0202	-40.
	GFF-44	EDM	3659	250.	0.0103	0.0217	0.0311	0.0189	-39.
	GFF-33	Fatigue	2836	235.	0.0067	0.0172	0.0256	0.0166	-35.
	GFF-34	Fatigue	2010	244.	0.0079	0.0125	0.0204	0.0143	-29.9
CS-19	PGN-10	EDM	464	13.6	0.0064	0.00640	0.0129	0.0113	-12.4
Aluminus	PGN-12	EDM	488	12.4	0.0066	0.00686	0.0133	0.0115	-13.5
	PGN-16	EDM	408	127	0.0055	0.00560	0.0123	0.0108	-12.2
	PGN-31	Fatigue	175	8.5	0.0022	0.00214	0.0099	0.0092	-7.6
	PGN-57	Fatigue	171	7.4	0.0028	0.00241	0.0099	0.0094	-6.7
	PGN-60	Fatigue	200	9.0	0.0029	0.00272	0.0102	0.0093	-7.2

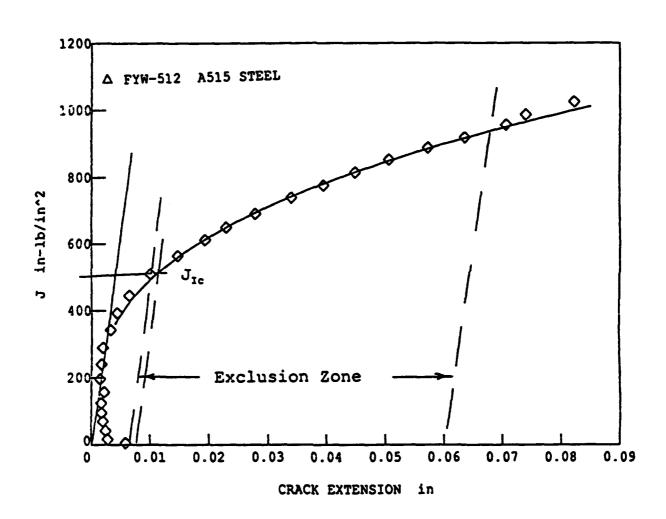


Figure 18 J_k evaluation for specimen FYW-512.

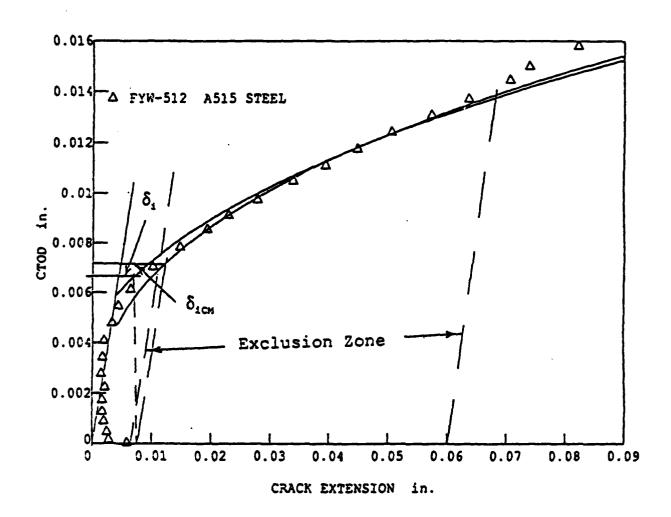


Figure 19 δ_i and δ_{iCM} comparison for specimen FYW-512.

Table 4 Comparison of average fracture toughness measured for EDM notched and fatigue precracked specimens.

Mandal		J _b (in-lb/is²)			δ _i (ia.)		δ _{ιΩε} (is.)				
Material	Patigos	EDM	% diff.	Petitus	EDM	% dift.	Fatigue	EDM	% 4ff.		
A302	648	254	36	0.0066	0.0093	41	0.0069	0.010	45		
A515	594	692	16	0.0068	0.0092	44	0.0061	0.0094	16		
A533B	1445	1987	38	0.0100	0.0135	35	0.0126	0.0171	36		
HY-100	706	947	34	0.0036	0.0053	47	0.0036	0.0052	43		
A710	2423	3861	59	0.0083	0.01	20	0.015	0.023	54		
C8-19	181	453	150	0.0028	0.0062	121	0.0026	0,0063	142		

Figure 20, it does not start to tear beyond blunting until approximately 0.4 mm of crack tip blunting has occurred (as indicated by the change in slope of the data in the early portion of the R curve). The definition of CTOD initiation proposed in the Common Method is (nearly - see below) consistent with the definition of J_{k} given in E813, and hence makes some allowance for blunting behavior by specifying that initiation is defined to occur at a fixed offset from the blunting line.

None of the fatigue precracked specimens had an initiation CTOD toughness that was on the order of 10 times the initial diameter of the EDM notch tip. The toughest materials, A533B and A710 had average $\delta_{\rm ICM}$'s of 0.0126 in. and 0.015 in., respectively, which is from 3.1 to 3.8 times the initial notch tip diameter. It is not clear that structural materials indeed exist which will demonstrate a $\delta_{\rm i}$, measured in any reasonable fashion, that is on the order of 0.040 in., and it certainly seems clear that weldments of this toughness are not a likely development in the near future. Thus, while the original hypothesis could not be verified, it seems clear that the use of EDM notches must be expected to result in higher initiation toughnesses, and if they are used to position a crack tip in a specific microstructure, some procedure would have to be used to correct the data for the presence of the EDM notch root radius.

It was expected that the tougher materials would show lower elevation than less tough

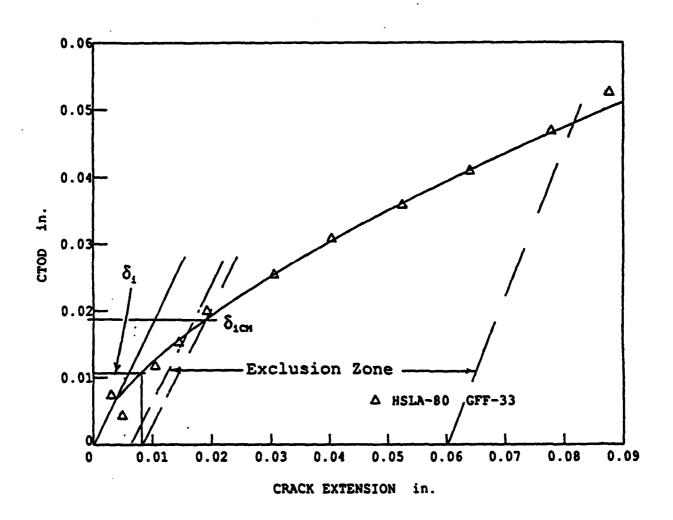


Figure 20 δ_i and δ_{iCM} comparison for specimen GFF-33.

materials. This trend was not observed in this investigation. The lowest toughness material, CS-19 aluminum, acted as expected by showing the greatest increase in toughness due to the EDM notch. For this material, the EDM notch tip diameter was approximately equal to the initiation toughness of a precracked specimen and the EDM notch specimen had an elevation on the order of 140% over the precracked specimen. The highest toughness materials, A533B and A710, showed smaller, but still substantial increases in crack initiation toughness (38% and 59% for J_k and 75% and 36% for δ_{kCM}). On the other hand, the A302 and A515 materials, with intermediate CTOD toughness, showed less sensitivity to the EDM notch, with increases in J_k of 36% and 16% respectively, and increases in δ_{kCM} of 45% and 16%. The HY-100 alloy, with the second lowest toughness in CTOD terms, shows the second lowest dependence on the notch tip radius.

The sensitivity of the initiation fracture toughness to the EDM notch does not seem to correlate with the strain hardening of the steel either. The HY-100 and A710 steel both have strain hardening exponents, N=15 and the tougher A710 showed a greater sensitivity to the EDM notch than the HY-100. On the other hand, the A302 and A533B both have N=9. For these two materials, the tougher A533B showed less sensitivity to the EDM notch than the A302. These conflicting trends indicate that there is not a one-to-one relationship between strain hardening and sensitivity of the fracture toughness to the presence of an EDM notch.

4.3 Improvement of the Common Method

The slope of the Common Method construction line that is used to evaluate $\delta_{\rm ICM}$ was set as 2.0, assuming a circular opening of the crack tip. Comparing the crack extension at crack initiation that results from this assumption with the crack initiation at $J_{\rm k}$ of E 813, as shown in Table 3, demonstrates that this definition of $\delta_{\rm ICM}$ is not very consistent with $J_{\rm k}$. An improvement can be made if work of Paris et. al.[2], Shih [3] or Rice et. al.[4] is used giving:

$$\frac{d\delta}{da} = \alpha \frac{\frac{dJ}{da}}{\sigma_f} \tag{12}$$

with $\alpha = 0.65$ to 0.7, and substituting dJ/da = $2\sigma_c$ gives

$$\frac{d\delta}{da} = 2\alpha = 1.3 - 1.4 \tag{13}$$

which implies that the slope of the δ blunting/construction line should have a slope of between 1.3 and 1.4 to be consistent with the slope of $2\sigma_{\ell}$ used by E813 and the Common Method for the case of bend type, plane strain test specimens. Recalculating $\delta_{\rm KM}$ using a construction line slope of 1.4 gives the results shown in Table 5. It is clear that the $\delta_{\rm KM}$ values have changed only slightly, but the crack extension at the initiation point has become much more consistent with that resulting from E813. The difference between the crack extension at $J_{\rm kc}$ and $\delta_{\rm kcM}$, however, is greatly reduced using the smaller construction line slope, with the differences being reduced from a maximum of 40% to a maximum of 12.5%.

Table 5 Comparison of Δa at initiation using construction line slopes of 2.0 and 1.4.

Material	Specimen ID	Notch Type	8 _{t04} (in.) Slope = 1 <i>A</i>	As at J. (in.)	Δa at δ _{icar} (in.)	% Difference
ASTM	FYX-511	EDM	0.0103	0.0145	0.0154	6.2
A302 Gr. B	FYX-S24	EDM	0.0108	0.0146	0.0158	8.2
	FYX-526	EDM	0.0113	0.0148	0.0161	8.8
	FYX-516	Fatigue	0.0066	0.0123	0.0129	4.9
	FYX-527	Fatigue	0.0012	0.0135	0.0140	3.7
ASTM	FYW-514	EDM	0.0088	0.0135	0.0144	6.7
A515 Gr. 70	FYW-516	EDM	0.0106	0.0149	0.0158	6.0
G. 75	FYW-512	Patigue	0.0074	0.0128	0.0134	4.7
	FYW-518	Patigue	0.0096	0.0139	0.0149	7.2
ASTM	A1	EDM	0.0170	0.0196	0.0201	1.5
A 533 Gr. B	A3	EDM	0.0211	0.0227	0.0232	2.2
	A4	EDM	0.0194	0.0210	0.0219	4.3
	Cl	Patigue	0.0129	0.0163	0.0173	6.3
	C3	Fetigue	0.0147	0.0183	0.0185	1.1
HY-100	FYO-2	EDM	0.0052	0.0120	0.0118	-1.7
	FYO-6	EDM	0.0049	0.0117	0.0116	-0.8
	FYO-8	EDM	0.0058	0.0126	0.0122	-3.2
	FYO-J3	Fatigue	0.0040	0.0113	0.0109	-3.5
	FYO-J4	Fatigue	0.0036	0.0109	0.0107	-1.8
:	FYO-150	Fatigue	0.0037	0.0111	0.0106	-2.7
	FYO-151	Fatigue	0.0038	0.0111	0.0106	-27
HSLA-80	GFF-42	EDM	0.0309	0.0339	0.0306	-9 .7
	GFF-44	EDM	0.0279	0.0311	0.0282	-9.3
j	GFF-33	Fetigue	0.0202	0.0256	0.0234	-12.5
	CIFF-34	Fatigue	0.0151	0.0204	0.0188	-7.8
CS-19	PGN-10	EDM	0.0066	0.0129	0.0128	-0.8
Alvaines	FGN-12	EDM	0.0070	0.0133	0.0131	-1.5
1	PGN-16	EDM	0.0056	0.0123	0.0121	-1.6
1	PON-31	Patigue	0.0022	0.0099	0.0097	-2.3
j	PGN-57	Fetigue	0.0023	0.0102	0.0101	-1.0
	PGN-60	Petigus	.0028	0.0100	90098	-1.5

5.0 CONCLUSIONS

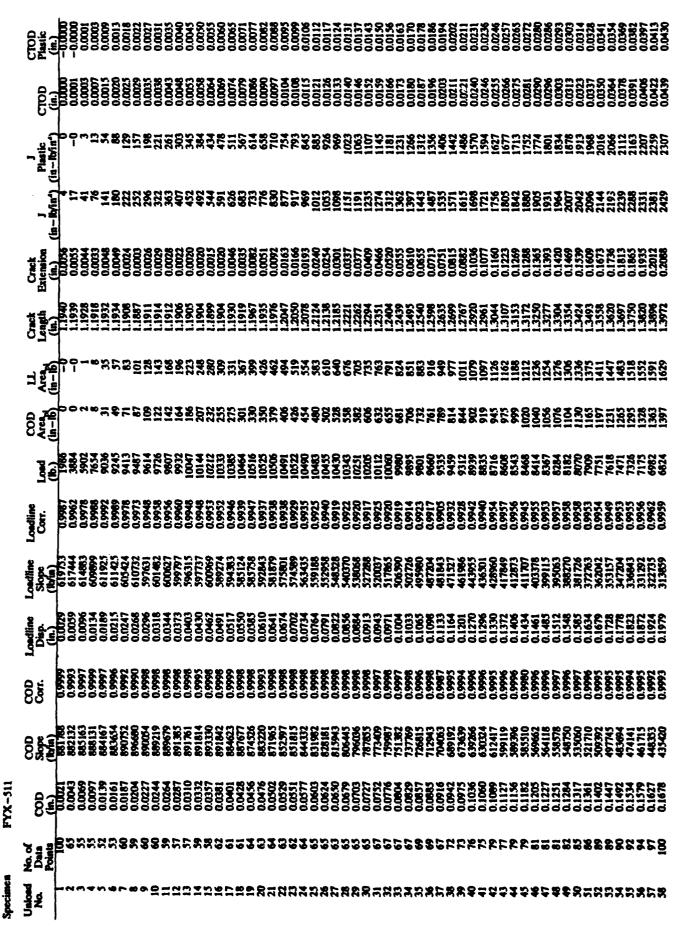
The following are the principal conclusions derived from this effort:

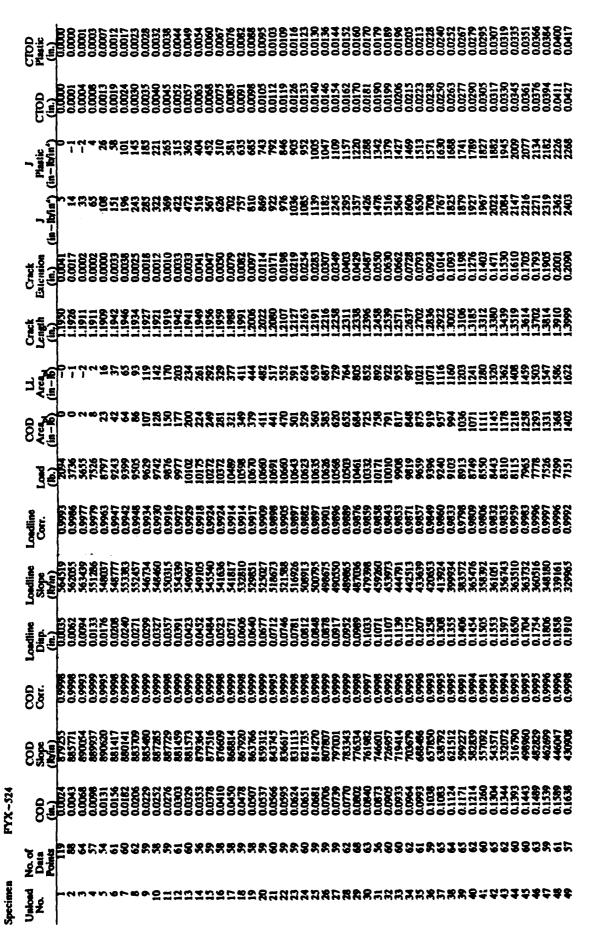
- 1) Wire EDM notches cannot be substituted for fatigue pre-cracks in fracture mechanics tests for any of the materials studied in this program without large changes in the measured initiation toughness resulting. The smallest EDM notch tip radii that could be cut were approximately 0.002 in. (0.05 mm) which was on the order of 1/5 the initiation CTOD measured using the Common Method technique. The original precept of the work was that structural materials with initiation CTOD values on the order of 6 to 10 times the initial notch radius would likely be independent of the initial notch or fatigue crack geometry. This precept was not fully tested since it was found that few, if any, structural materials were tough enough to meet this criterion.
- A pattern relating the initiation toughness notch geometry to material toughness was not found in this work. High toughness alone did not seem to make a material less sensitive to the initial crack tip geometry. Some materials were much more sensitive to the initial notch radius, but it was not necessarily the less tough materials that were the more sensitive.
- 3) The J-R curves slope, and the general shape of both the J-R and δ-R curves seemed quite insensitive to the type of notch geometry present in the specimen. If ductile tearing instability was the mode of failure of principal interest, then the use of EDM notches might be practical.
- In general, if EDM notches were to be used, a research study is necessary to evaluate the effects of the blunt notches, and in all likelihood a correction would be necessary to estimate the true J_k , δ_i , or resistance curve that would be present if fatigue cracks existed in the structural application.

5) The initiation CTOD method of the ASTM E24.08.01 Common Method is strongly preferred in comparison with that of ASTM E1290. The E1290 method arbitrarily shortchanges the tougher materials by assuming that the onset of ductile tearing always occurs at 0.2 mm or 0.008 inches. The results of this work show that this is certainly not the case. The offset blunting line method of the Common Method document seems to give an initiation point consistent with the J_k measurement point of ASTM E813. A modification of the Common Method construction line slope is recommended, based on these results, which improves the correspondence between J_k and the Common Method δ_i.

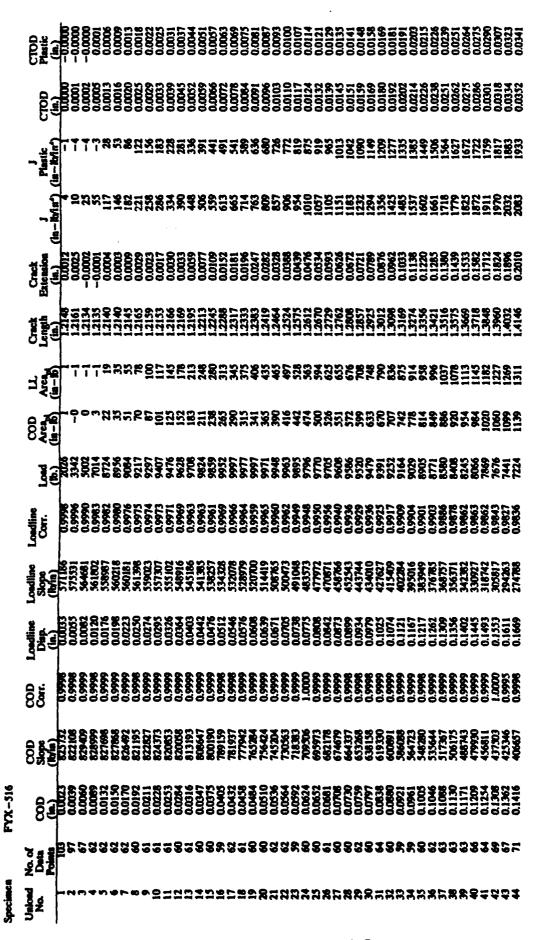
APPENDIX A

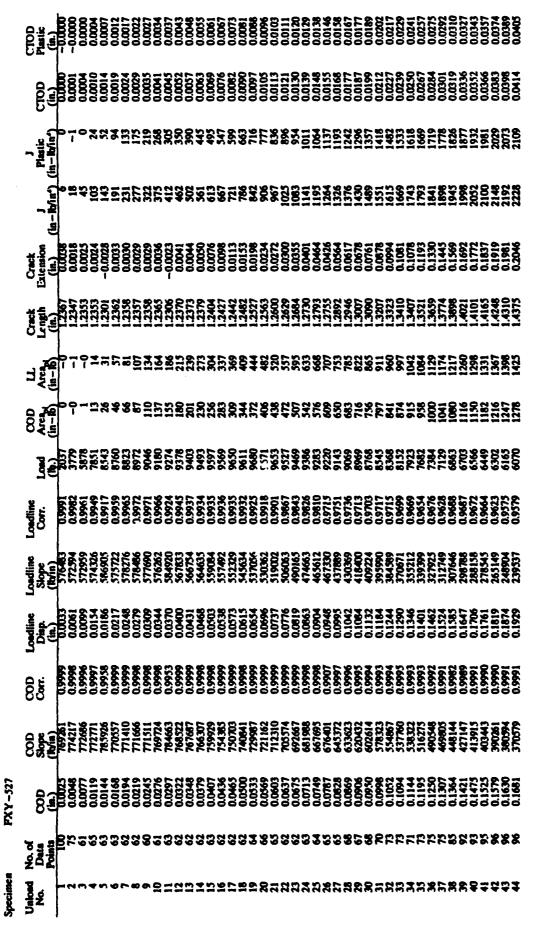
Data Tables for Individual Specimens

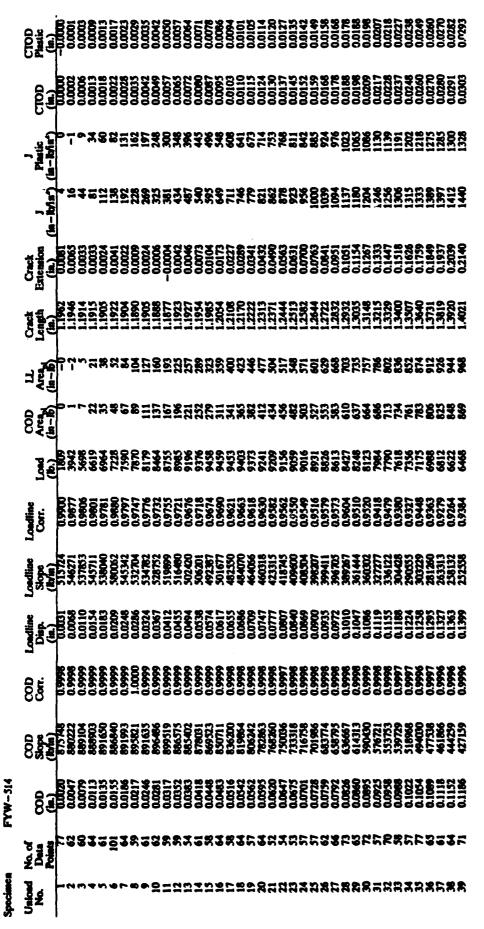


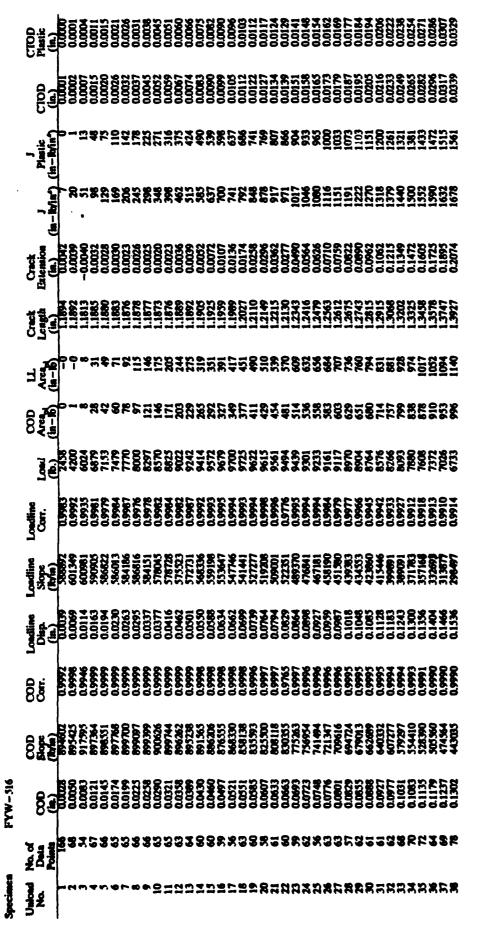


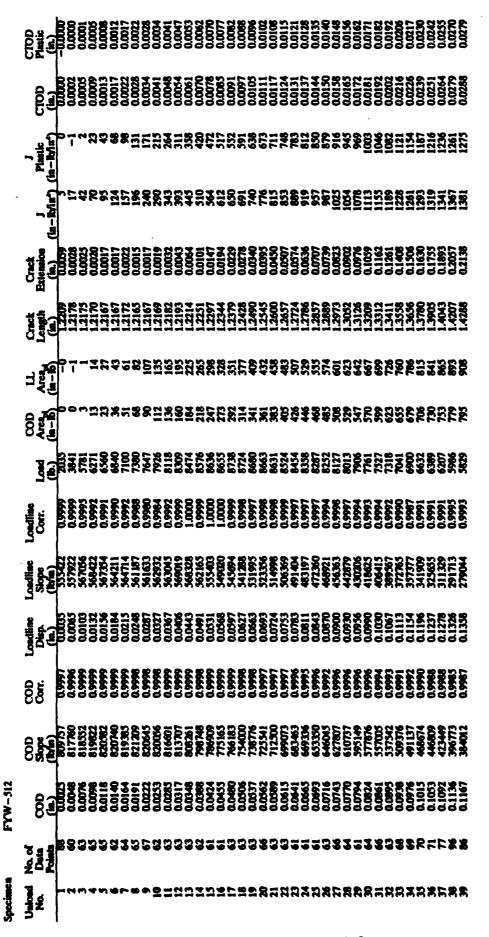
	CTOD Plastic (in.)	00000	0.000	9000	0.0020	0.0027	0.0039	900	0.0061	0.00	0.0064	0.00	0.0105	0.011	0.0126	0.0134	0.0150	0.0158 0.0158	0.017	0.00	0.0203	0.0224	0.0231	0.0250	0.0263	0.0287	0.0301	0.0330	0.0361	0.0392	0.0425
	CTOD €.	0.000	0.0003	0:00 7 7 7	0.0027	0.00 2000 2000 2000	0.0047	0000	0.0069	0.00	0.0092	0.0100	0.0114	0.0120	0.0136	0.01	0.0159	0.0168	0.0187	0.020	0.0215	0.0234	0.0242	0.0260	0.0273	0.0298	0.0312	0.0340	0.0371	0.00	0.0434
	J Plastic in – Min²)	P-	7 =	2 2	32	183	22	33	\$	2 .	3	25	814	50 50 50 50 50 50 50 50 50 50 50 50 50 5	25		=	1260	1320	1433	95	1576	1621 1631	1740	1835	88	2003 2003	2060	2139	2219	2285
	J Ga-Ibhar	v 73	¥ 28	25	î	275		56	\$	35	192	82	23	<u> </u>	8	1159	1212	1327	1435	151	161 183	1716	1762	1878	226	502	2063 2140	2194	227	2355	2418
	Crack Extension (in.)	0.0051	0.0020	0.0031	-0.000	0.0000	0.0038	0.00	000	0.0053	0.0072	0.000	0.0152	0.0181	0.0253	0.0289	0.0359	0.0403	0.0511	0.0526	0.0674	0.0801	0.0840	0.0693	0.1009	0.1162	0.1247	0.1401	0.1619	0.1830	0.2043
	Crack [in.]	1.1947	1.1916 1.1932	1.1927	1.1891	1.1901	1.1934	1.1938	1.194	1.1948	1.1967	1.1936	7048	12076	12149	12184	1.2254	1238	12406	12519	1.2570	1.2696	1.2735	1.2789	1.2904	1.3057	13142	1,3296	13514	272	13939
	7 \$ € 1 \$ €	0 -		23	3.55	25	33	217	8	378	421	\$ \$	232	<u> </u>	3	678 715	23	8 % 8 %	878	926	<u>8</u> 5	100	85	122	1213	1295	1383	1427	200	<u> </u>	1656
	Q ¥ €	Po	N 80	24	7	<u> </u>	3 <u>5</u>	181	25	314	200		7	\$5	Š	88	8	3 5	25.	810	3 5	3	8 8 8	8	<u>8</u> 6	9	260	1230	8	15.5 15.5 15.5 15.5 15.5 15.5 15.5 15.5	4
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	Londline Corr.	0000 1.0000	0.9999	0.9999	0.9968	0.999	0.994	0.9997	0.6660	0.9996	0.9998	0.9992	0.9996	0.9997	0.9998	9666 5066 5066	0.9998	0.9998	0.9996	0.9996	0,999	0.9999	0666°C	0.9981	0.9998	0.999	8666 6666 6666 6666 6666	0.9998 0.9998	0.999	0.9999	0.9998
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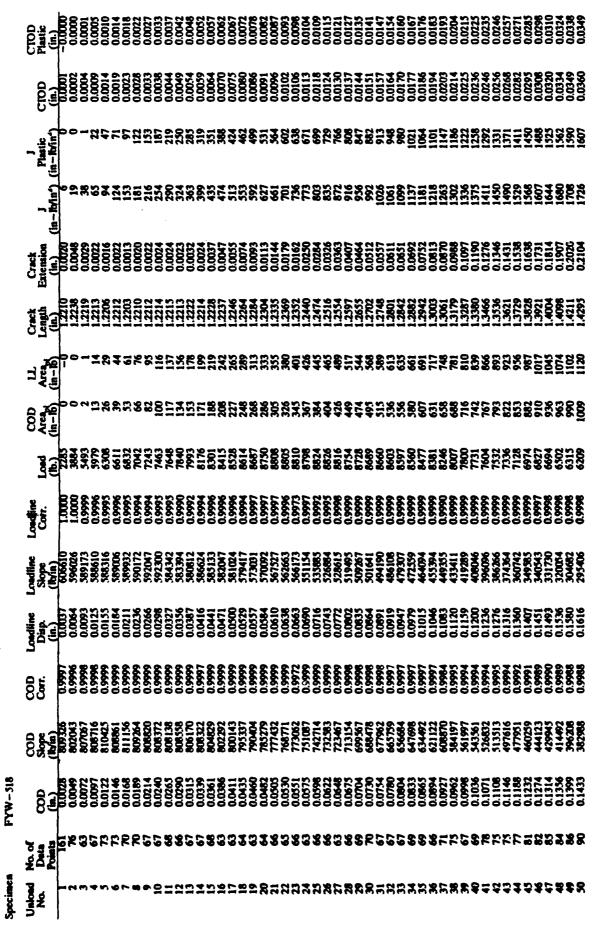


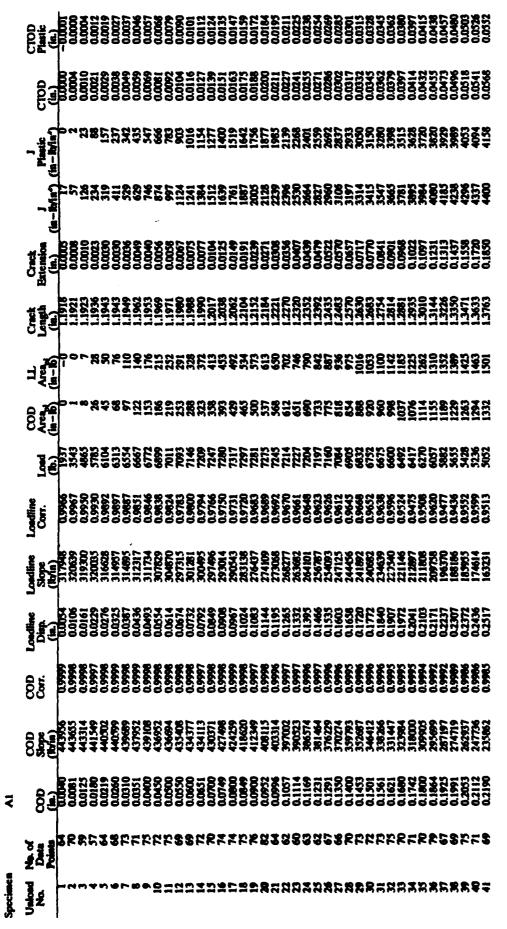


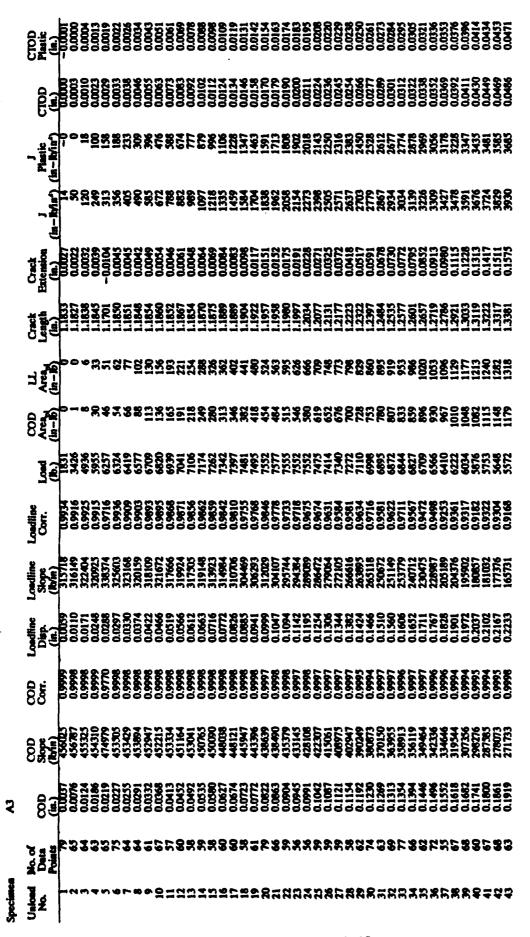


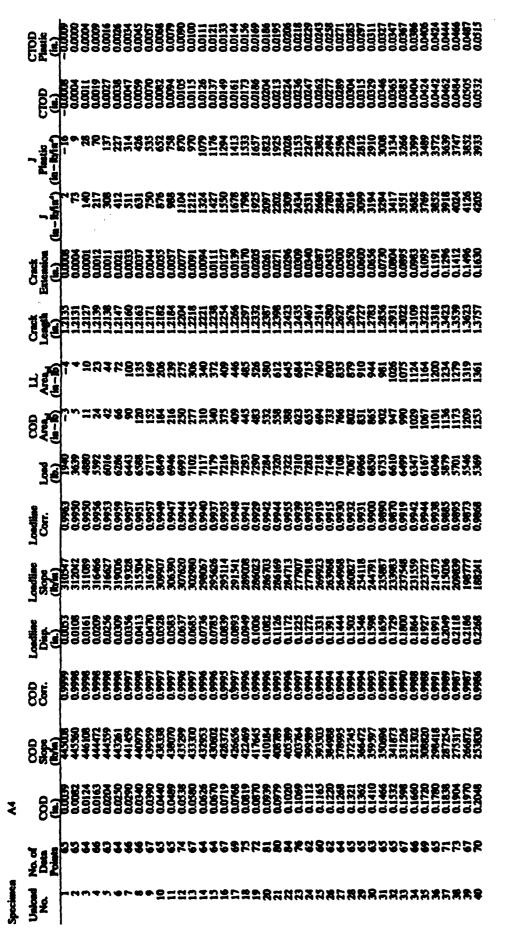


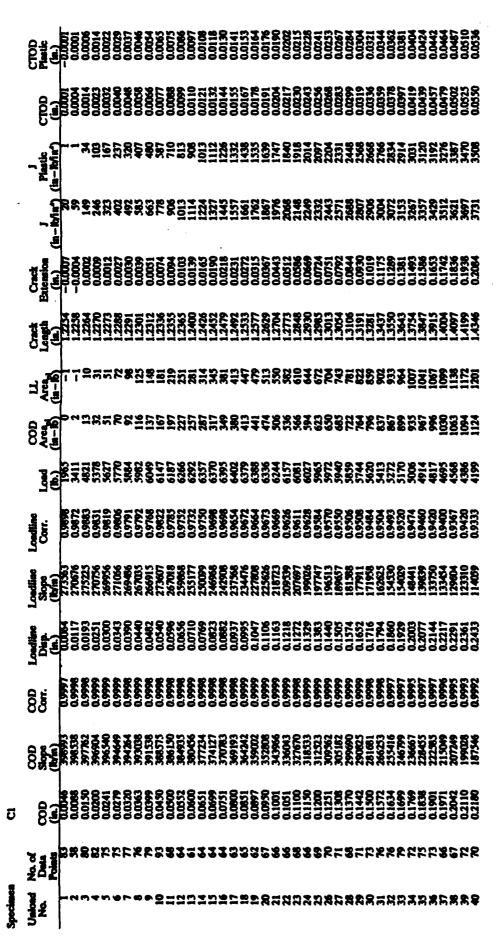


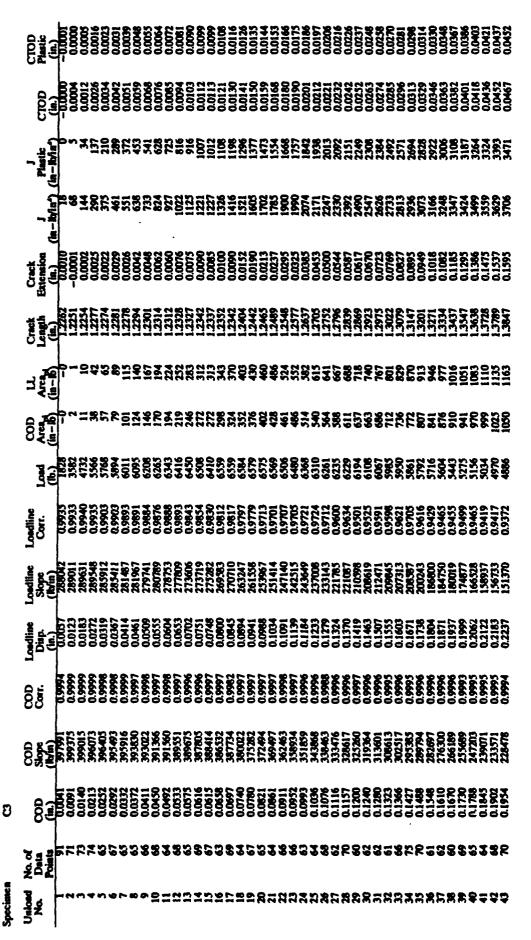


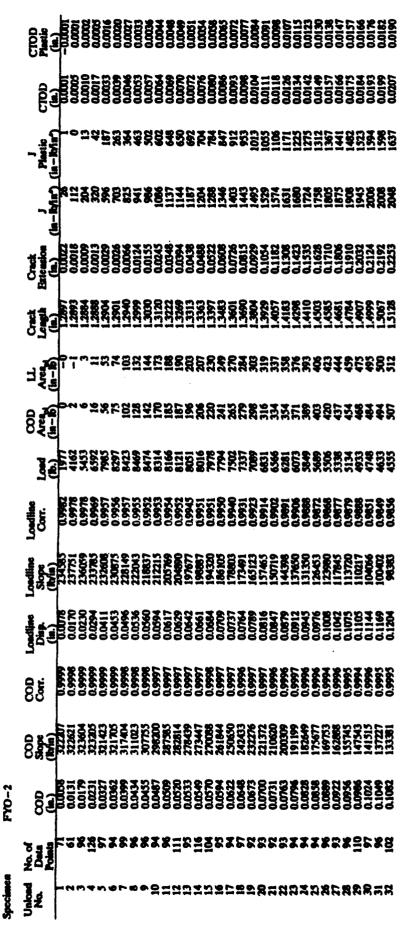


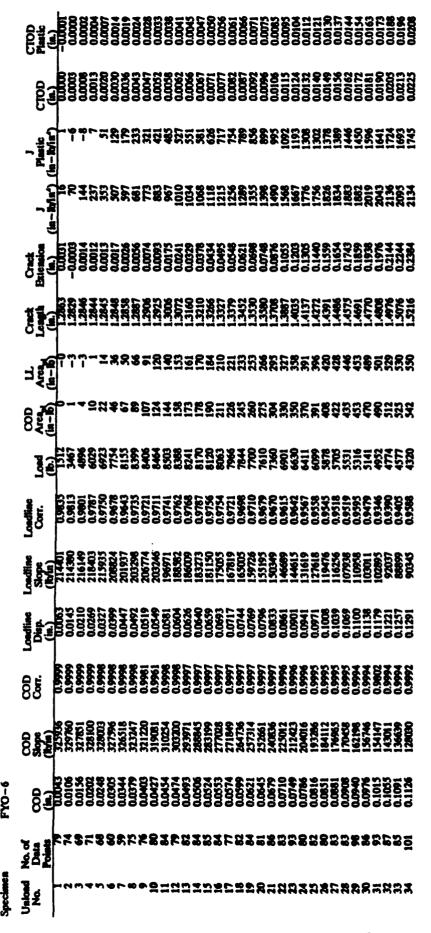




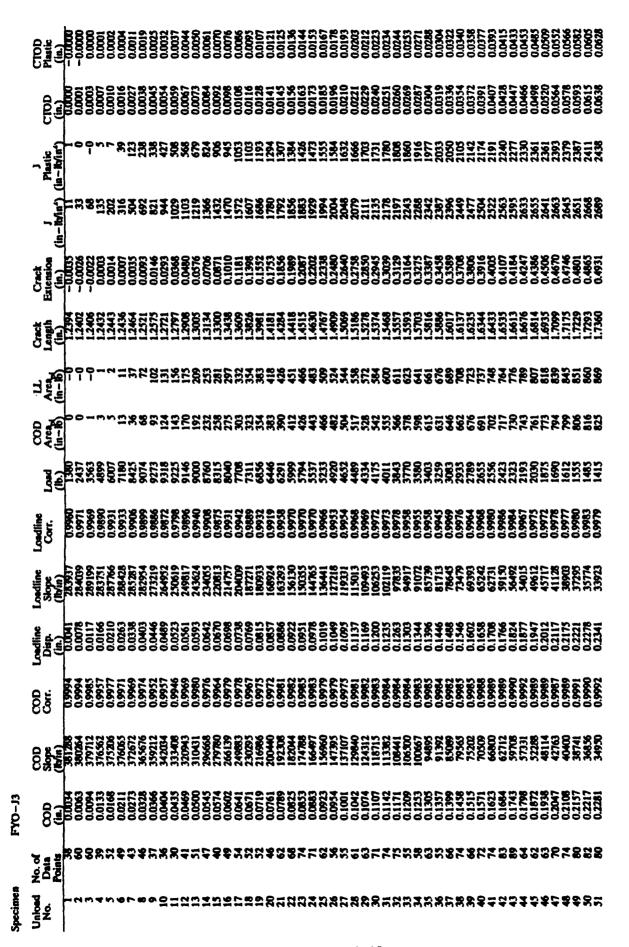


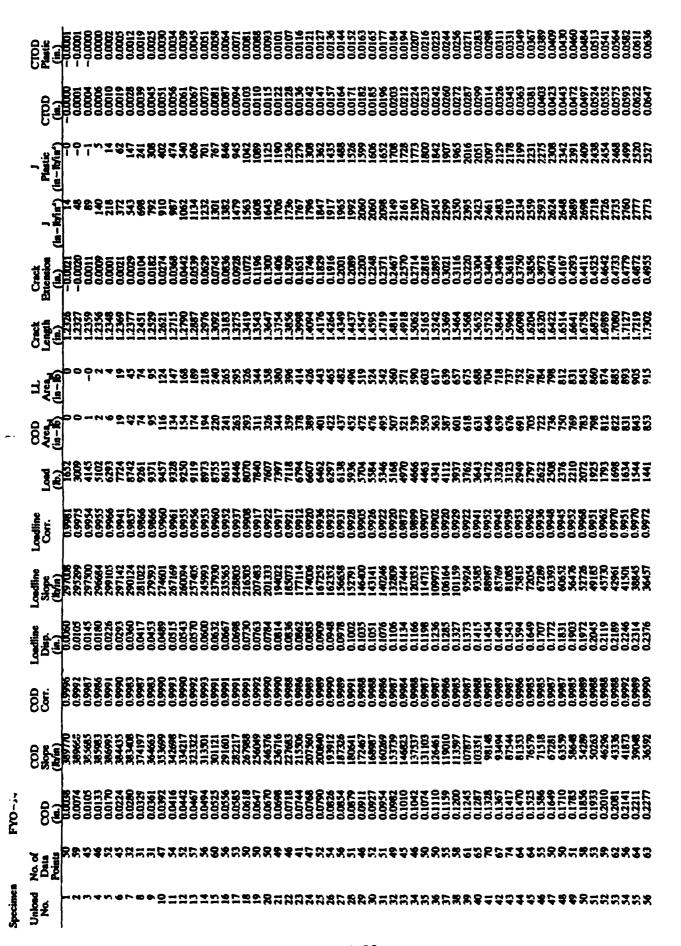


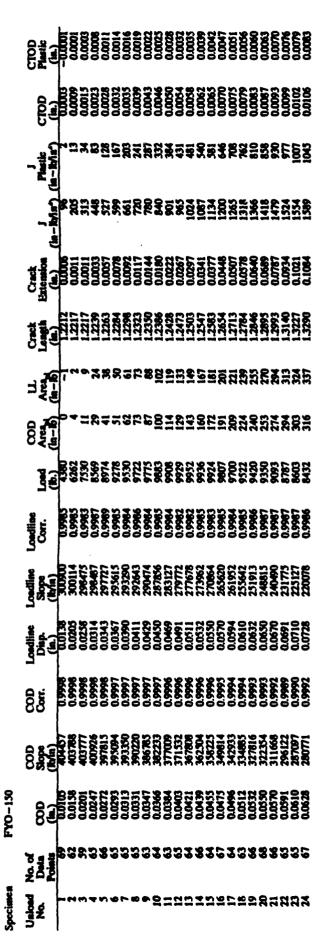


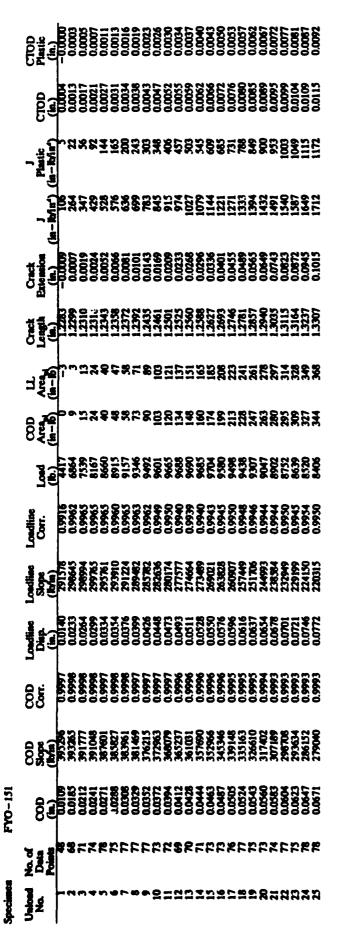


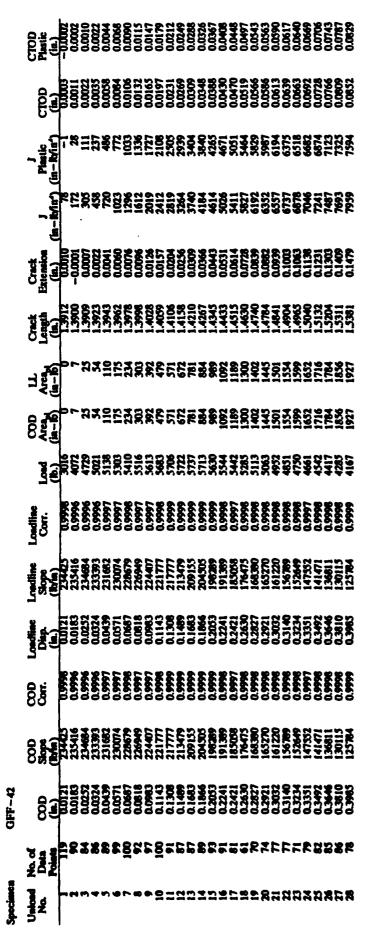
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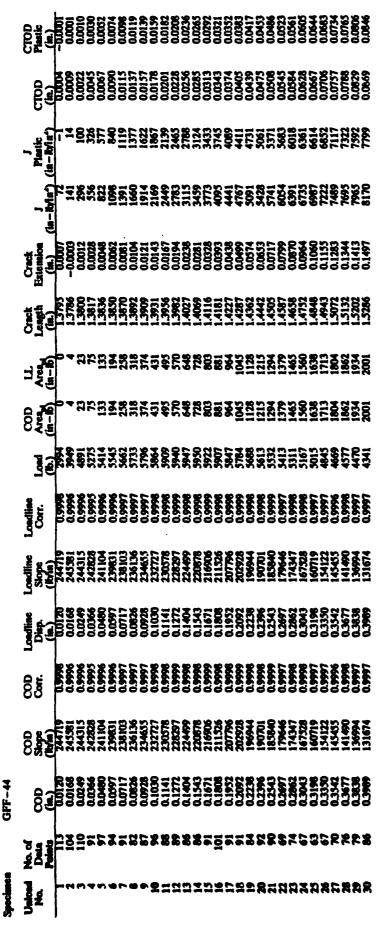


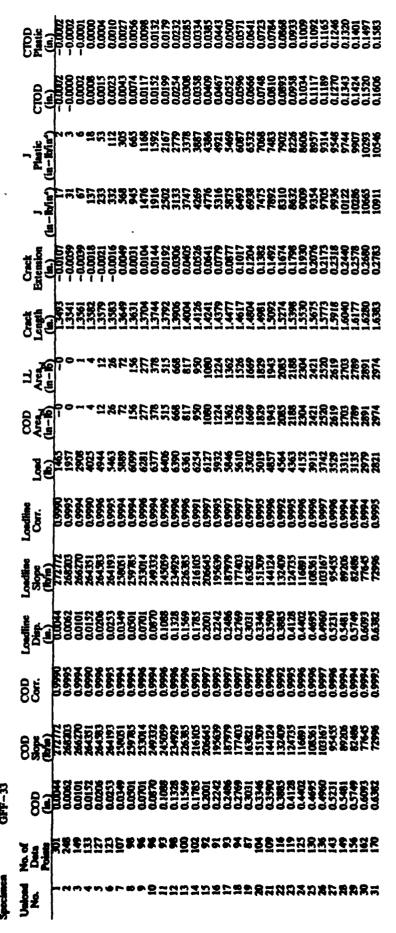


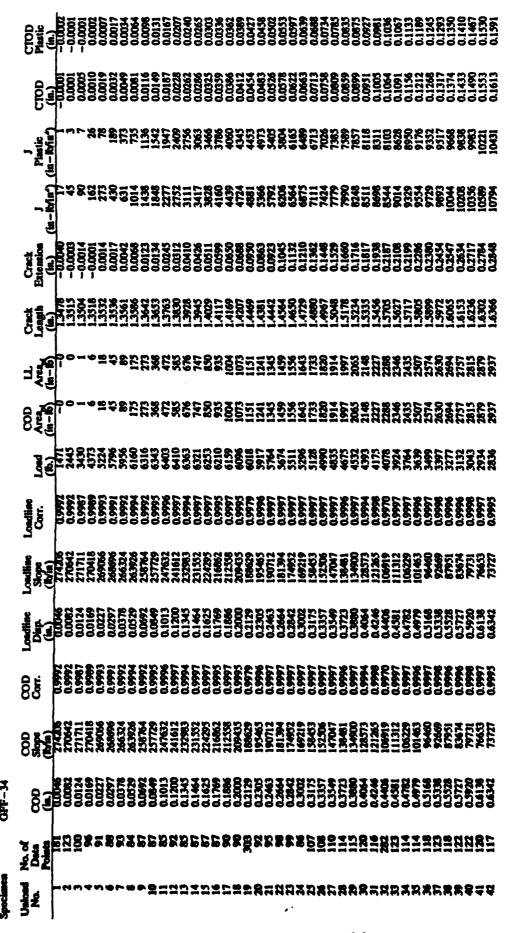


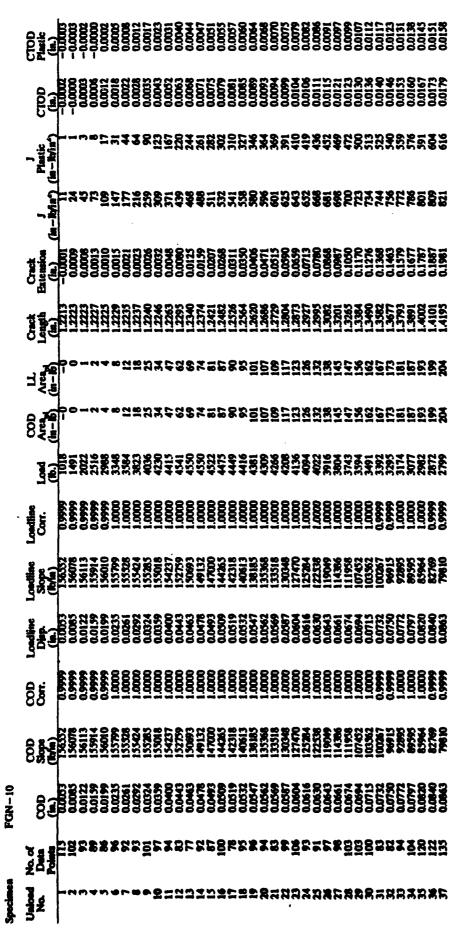


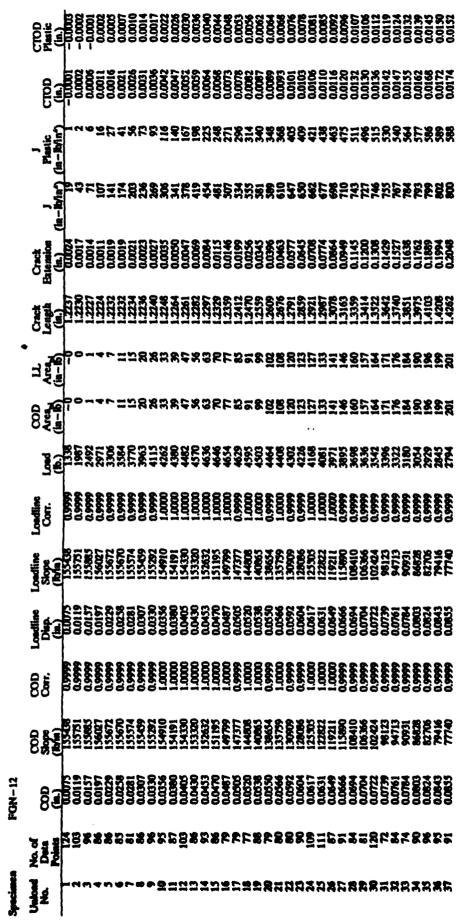


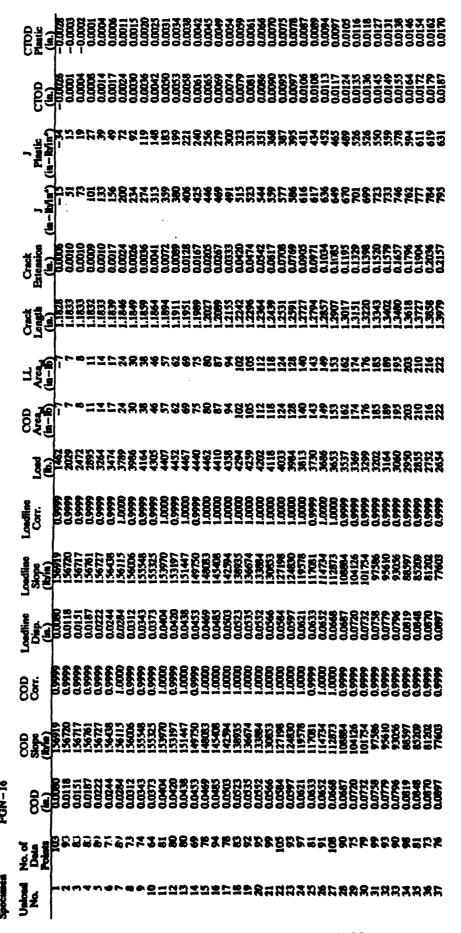


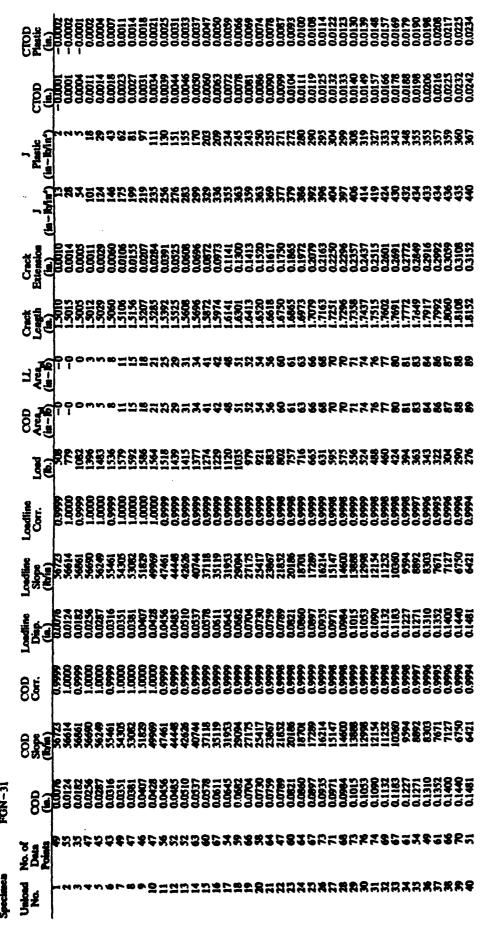


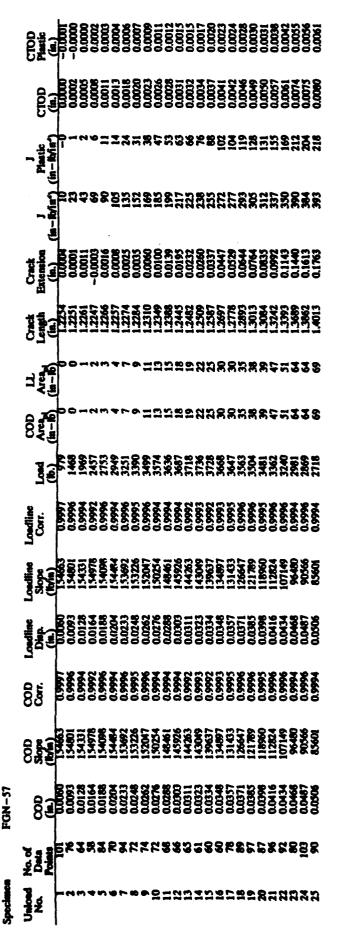


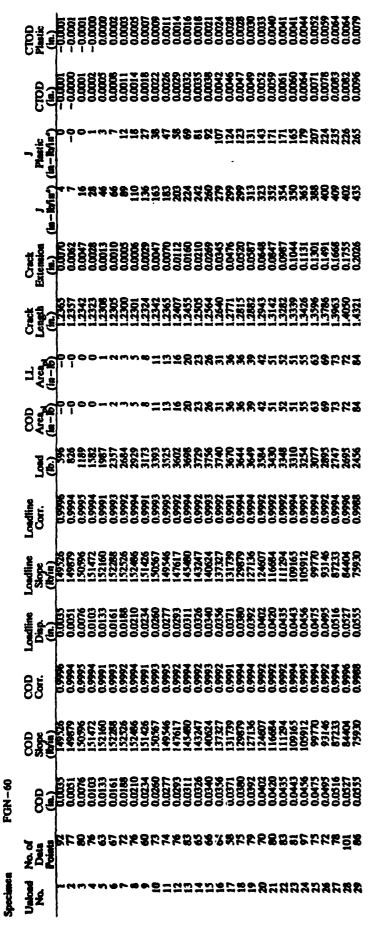












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1. AGENCY USE ONLY (Leave blank)	1. AGENCY USE ONLY (Leave blank) 2. REPORT DATE 3. REPORT TYP						
•	APR 1993	FINAL					
4. TITLE AND SUBTITLE The Effect of Electric on the Fracture Toughne			5. FUNDING NUMBERS 1-2814-554				
6. AUTHOR(S)			1-2814-653				
J.A. Joyce and R.E. Lin							
7. PERFORMING ORGANIZATION NAME	(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION REPORT NUMBER				
US Naval Academy			CRDKNSWC				
Annapolis Maryland 214	02		SSM-61-93-01				
Carderock Div, Naval Su			1				
Annapolis, MD 21402-506	7						
9. SPONSORING/MONITORING AGENCY	NAME(S) AND ADDRESS(ES)		10. SPONSORING / MONITORING AGENCY REPORT NUMBER				
US Nuclear Regulatory C	ommision		NUREG/CR-5981				
Washington DC 20555							
11. SUPPLEMENTARY NOTES							
12a DISTRIBUTION AVAILABILITY STATE Distribution: Approved is unlimited		distribution	12b. DISTRIBUTION CODE				

13. ABSTRACT (Maximum 200 words)

Recent computational studies of the stress and strain fields at the tip of very sharp notches have shown that the stress and strain fields are very weakly dependent on the initial geometry of the notch once the notch has been blunted to a radius that is 6 to 10 times the initial root radius. It follows that if the fracture toughness of a material is sufficiently high so that fracture initiation does not occur in a specimen until the crack-tip opening displacement (CTOD) reaches a value from 6 to 10 times the size of the initial notch tip diameter, then the fracture toughness will be independent of whether a fatigue crack or a machined notch served as the initial crack. In this experimental program the fracture toughness (J_k and J resistance (J-R) curve, and CTOD) for several structural alloys was measured using specimens with conventional fatigue cracks and with EDM machined notches. The results of this program have shown, in fact, that most structural materials do not achieve initiation CTOD values on the order of 6 to 10 times the radius of even the smallest EDM notch tip presently achievable.

Unclassified	Unclassified	Unclassified	Same as Report
17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFICATION OF ABSTRACT	20. LIMITATION OF ABS
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14. SUBJECT TERMS Jie, J R curve, cons	traint, crack-tip open	ing displacement	15. NUMBER OF PAGES